

## The mechanical and electrical characteristics of PVA:PVP mix films reinforced with cadmium chloride

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**Abstract:** Using the casting process, this work created films with salt ( $\text{CdCl}_2 \cdot \text{H}_2\text{O}$ ) reinforced polymer blends and pure polymer blends (PVA:PVP) at various weight ratios (10 wt%, 20 wt%, 40 wt%). Experimental results demonstrated that the dielectric constant and dielectric loss factor for all polymer blend films decreased with increasing frequency, indicating that the dielectric properties of the films were affected by the salt weight ratio. The films were reinforced with  $\text{CdCl}_2 \cdot \text{H}_2\text{O}$  salt. There was a frequency-dependent rise in the aforementioned properties as the salt weight ratio rose. For all films containing a polymer mix, the testing findings demonstrated that AC electrical conductivity rose with frequency, and for the same frequency, it increased with salt weight ratio. A study was also conducted to examine the impact of salt weight ratio on the mechanical characteristics of films made of a salt-reinforced PVA:PVP polymer mix. The films made of salt-reinforced polymer blends showed interesting behaviour in the tensile test. As the salt weight ratio increased, the elongation at break, Young's modulus, and tensile strength all changed significantly. On the other hand, the hardness value went up and down, and the fracture energy value went up, suggesting that these films could be useful as rigid adhesives with limited flexibility.

### I. Introduction

Polymers such as plastics and rubbers pervade our lives, and we come across them in many different forms. Their physical properties are therefore of great importance, and an understanding of them is vital for their use in technology and engineering [1]. The blending of different polymers or inorganic materials with polymers represents a strategic route to improving the performance of a material, and allows the realization of novel composite systems that enhance the performance of the parent blend [2]. Polyvinyl alcohol (PVA) is a versatile, poly-hydroxy polymeric material which has gained the interest of researchers due to its many potential applications, and the scope for easy modification and formation of useful miscible blends with many other polymers. PVA reinforced with different materials like iodine, ferric chloride, barium chloride and other salts have been studied extensively, and these polymeric materials show a significant modification in their microstructural, electrical and mechanical properties when compared to pure PVA films [3]. The subject of polymer blends has been

2 3 4 5 6  
Log (Frequency (Hz))

Log-Log plot of the dielectric constant as a function of frequency. The plot shows the dielectric constant on the y-axis and the logarithm of frequency (Hz) on the x-axis, ranging from 2 to 6. The plot is used to study the frequency dependence of the dielectric constant for the prepared films.

lications through property enhancement and economic benefits. The blending of two or more polymers of similar or dissimilar natures has been practiced for many years [5]. Solution blending of different polymers is one of the methods used to obtain new material with a variety of properties, which mainly depend on the characteristics of the parent homo polymers and the blend composition [6]. Polyvinyl alcohol (PVA), a semi-crystalline polymer, has been studied widely because of its many interesting physical properties, which arise from the presence of OH groups and the hydrogen bond formation with other polymers or metals. Polyvinyl pyrrolidone (PVP) is a vinyl polymer possessing planar and highly polar side groups due to the peptide bond [7]. The aim of this study is to prepare pure polymer blend (PVA:PVP) film and salt ( $\text{CdCl}_2 \cdot \text{H}_2\text{O}$ ) reinforced polymer blend films at different weight ratios (10 wt%, 20 wt%, 40 wt%) using the casting method, and to investigate the effect of salt reinforcement on the dielectric and mechanical properties of the prepared films.

## II. Experimental work

In the preparation of polymer blend films, polyvinyl alcohol powder (produced by Central House (P) Ltd of India with a molecular weight of 13000 g/mol - 23000 g/mol), and Polyvinyl Pyrrolidone powder (produced by the Indian HIMEDIA Company, with a molecular weight of 40000 g/mol) were used. For reinforcement of the blend, cadmium chloride ( $\text{CdCl}_2 \cdot \text{H}_2\text{O}$ ) salt (produced by the Indian HIMEDIA Company) was used.

function of the frequency of pure and PVA:PVP poly-mer blend films reinforced with different weight ratios of  $\text{CdCl}_2 \cdot \text{H}_2\text{O}$  salt.

Pure PVA:PVP polymer blend film and  $\text{CdCl}_2 \cdot \text{H}_2\text{O}$  salt-reinforced polymer blend films were prepared at different weight ratios (10 wt%, 20 wt%, 40 wt%) using the casting method. The Differential Scanning Colorimeter (DSC) was performed for all samples and reported elsewhere, and the evidence for the blend nature of the film was confirmed [8]. The PVA and PVP powders with 1 : 1 wt%, and  $\text{CdCl}_2 \cdot \text{H}_2\text{O}$  powder with the above mentioned weight ratios were dissolved in distilled water by stirring for 1 hr at 60 .The solution was then poured into special glass molds placed on a flat surface and left until the solvent evaporated to obtain the pure polymer blend film and salt-reinforced polymer blend films. The thickness was measured using a digitalmicrometer, and was found to be in the range 1450  $\mu\text{m}$  - 1455  $\mu\text{m}$ . For the purpose of dielectricmeasurements, an LCR meter (4294A Agilent Precision Impedance Analyzer) was used in the frequency range of 100 Hz - 1 MHz at room tem- perature, and for the investigation of mechanical properties, the following instruments were used: Tinius Olsen-H10K for the tensile test, Shore D Checkline-dd-100 for the hardness test and FillingDarter Impact Tester of the type FDI-01 for the shock resistance test. Figure 1 shows the sample images required for each test.

Loss Factor (  $\epsilon''$  )

250

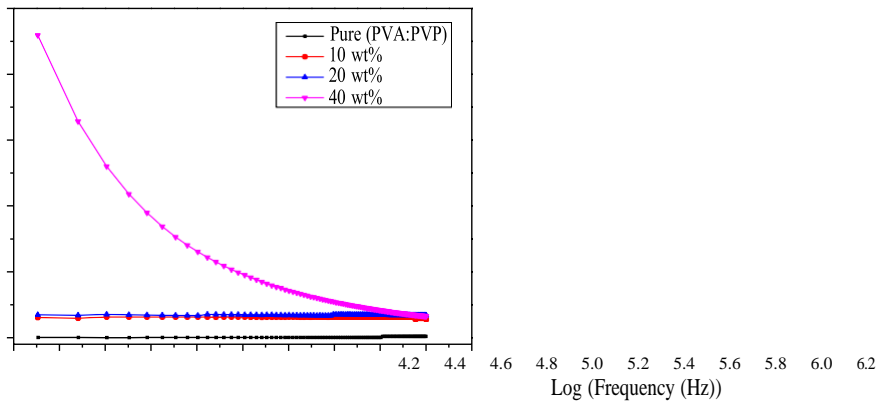
200

150

100

50

0



b

Log ( <sub>a.c.</sub> (S/m))

-2.5  
-3.0  
-3.5  
-4.0  
-4.5  
-5.0  
-5.5  
-6.0  
-6.5  
-7.0  
-7.5  
-8.0

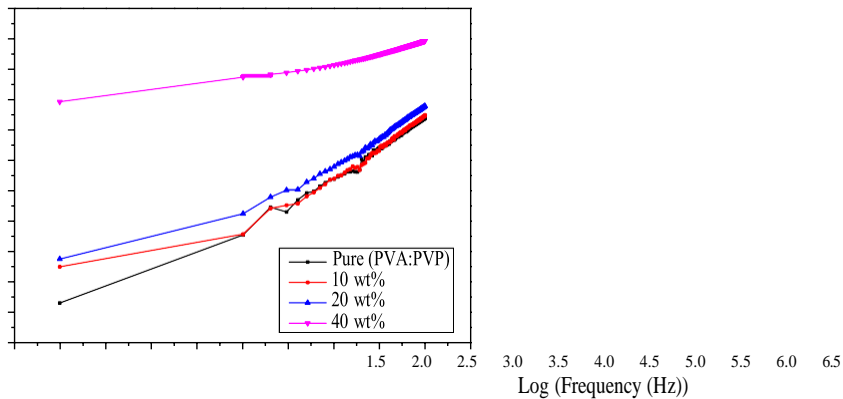


Figure 3: Semi-log plot of the loss factor as a function of the frequency of pure and PVA:PVP polymer blend films reinforced with different weight ratios of  $\text{CdCl}_2 \cdot \text{H}_2\text{O}$  salt.

### III. Results and discussion

#### i. Electrical properties

##### a. Dielectric constant

The dielectric constant ( $\epsilon'$ ) was recorded for pure polymer blend PVA:PVP film and  $\text{CdCl}_2 \cdot \text{H}_2\text{O}$  salt reinforced polymer blend films at different weight ratios (10 wt%, 20 wt%, 40 wt%) at room temperature and within the frequency range of 100 Hz - 1 MHz, as shown in Fig. 2. The dielectric constant decreased with increased frequency for all polymer blend films, which can be explained as follows:

In the low frequency region there will be sufficient time for molecular dipoles to rearrange and align themselves in the direction of the external electric field, but at high frequencies the time is shorter, and less than the time period needed by the molecules for rearrangement in the direction of the external electric field [9]. The dielectric constant at the same frequency increased with an increase in the weight ratio of added salt. In general, this increase in the value of the dielectric constant is due to increased polarization [10].

##### b. Loss factor

The loss factor ( $\epsilon''$ ) is the ratio of loss of power in electrically insulating materials to the total capacity transported through the insulator; i.e., the loss

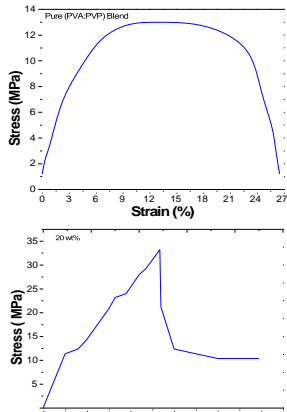
Figure 4: Log-log plot of A.C. electrical conductivity as a function of the frequency of pure and PVA:PVP polymer blend films reinforced with different weight ratios of  $\text{CdCl}_2 \cdot \text{H}_2\text{O}$  salt.

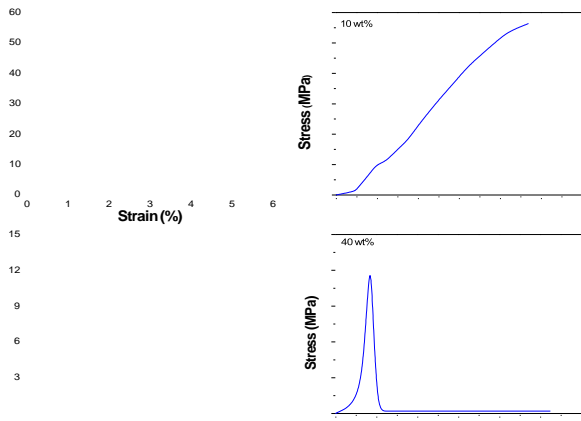
of energy in the insulating material is directly proportional to the loss factor. The dielectric loss factor of the pure PVA:PVP polymer blend films and polymer blend films reinforced by  $\text{CdCl}_2 \cdot \text{H}_2\text{O}$  salt was calculated at different weight ratios (10 wt%, 20 wt%, 40 wt%) at room temperature and within the frequency range of 100 Hz – 1 MHz, as shown in Fig. 3. It can be observed that the loss factor decreases as the frequency increases for all the polymer blend films. This may be attributed to the enhancement of the charge carriers that takes place across the electric charge area, decreasing the value of the loss factor at high frequencies until the electron's energy is equal to the Fermi level [11]. Another reason for the change in the loss factor with frequency is the polarization mechanism and the multiple interactions between ions and dipoles. This is due to the value of relaxation time [12]. It is also observed that the value of the loss factor at the same frequency increases with an increase in the weight ratio of the added salt. In general, this increase in the value of the dielectric loss factor is attributed to the increase in polarization and the increase in ion charge carriers [13, 14].

### *c. AC electrical conductivity*

The alternating electrical conductivity of the pure PVA:PVP polymer blend films and polymer blend films reinforced by  $\text{CdCl}_2 \cdot \text{H}_2\text{O}$  salt was measured







**ii. Mechanical properties**

*a. Tensile test*

The tensile test was conducted and stress-strain curves were obtained for pure PVA:PVP polymer blend films and polymer blend films reinforced by CdCl<sub>2</sub> H<sub>2</sub>O salt at different weight ratios (10 wt%, 20 wt%, 40 wt%) . These curves are shown in Fig.

5. The stress-strain of the pure polymer blend films consists of the elastic deformation region showing a linear relationship between stress and strain. From this region Young's modulus can be estimated from

0 1 2 3 4 5  
Strain (%)

°  
0.0

0.5

1.0 1.5 2.0 2.5 3.0  
**Strain (%)**

the slope of the straight line. The polymeric material within the boundaries of this region suffers from an elastic deformation due to the stretching and elongation of the polymeric chains without break-

Figure 5: Stress-strain curves of pure and PVA:PVP polymer blend films reinforced with different weight ratios of  $\text{CdCl}_2 \cdot \text{H}_2\text{O}$  salt.

at different weight ratios (10 wt%, 20 wt%, 40 wt%) at room temperature and within the frequency range of 100 Hz - 1 MHz, as shown in Fig. 4. It is clear that the alternating electrical conductivity increases significantly as the frequency increases for all the polymer blend films, and this increase is due to increased polarization in the samples [15]. It should be noted that the alternating electrical conductivity in a dielectric material is the amount of power lost when an alternating electric field is exerted, which appears as heat when the dipoles rotate in their positions. The vibration of the charges changes with the alternating electric field, and therefore depends on the frequency [16]. Moreover, the alternating electrical conductivity at the same frequency increases with an increase in the weight ratio of added salt. This increase is strongly affected by many factors, including the purity of the material and dispersion. In general, this increase in alternating electrical conductivity is attributed to a decrease in dielectric resistance due to the increase of conductive molecules in the polymeric blend films [17], and also because of the number of charge carriers that have a significant relaxation time due to the high energy barrier [18].

ing the bonds. This curve deviates from linear behavior due to cracks generated within the polymeric material. These cracks grow and combine with increased stress, creating larger incisions and continuing to grow with stress until a fracture occurs in the sample [19]. In other cases, the fracture begins at the outer surfaces in the sites of deformities or defects such as scratches, holes or internal cracks, which act as areas for concentration of stress. This leads to a rise in the stress value to limits where the strength value exceeds the internal force of cohesion, and thus breakage occurs.

When the  $\text{CdCl}_2 \cdot \text{H}_2\text{O}$  salt is added to the pure polymer blend, the stress-strain curve changes and we obtain curves with different properties. Figures 6, 7 and 8 show the variations in tensile strength,

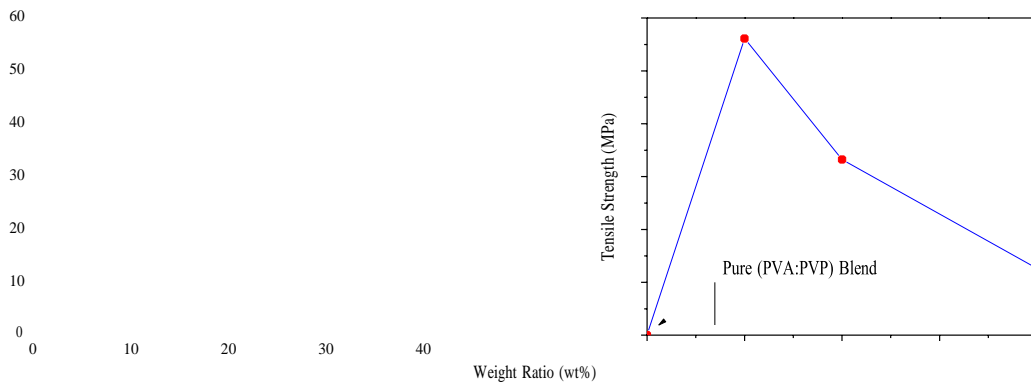


Figure 6: Tensile strength of pure and PVA:PVP polymer blend films reinforced with different weight ratios of  $\text{CdCl}_2 \cdot \text{H}_2\text{O}$  salt.



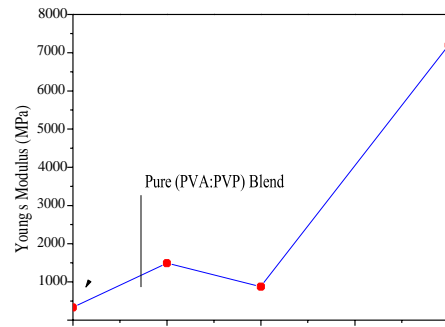
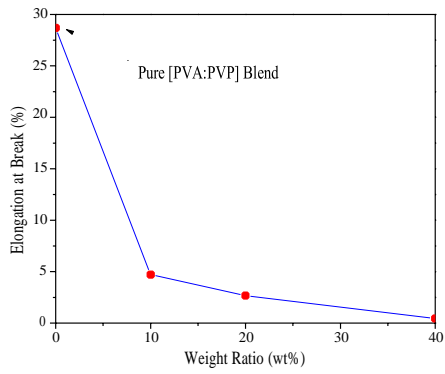




Figure 7: Elongation at break of pure and PVA:PVP polymer blend films reinforced with different weight ratios of CdCl<sub>2</sub>·H<sub>2</sub>O salt.

elongation at break and Young’s modulus as a function of the weight ratio of the added salt, for all samples. Table 1 shows the values of tensile strength, elongation at break and Young’s modulus for all polymer films, determined from the stress-strain curves. The tensile strength of the pure polymer blend films is 15.5 MPa, the elongation at break value is 28.7 % and the value of Young’s modulus is 332 MPa; however, when the blend is reinforced with CdCl<sub>2</sub>·H<sub>2</sub>O salt, these values change. The tensile strength values increase at the 10 wt% weight ratio, reaching 56.1 MPa, and then decrease with an increase in the weight ratio of the salt added. The elongation at break value starts to decrease with an increase in the weight ratio of salt added, while the value of Young’s modulus starts to increase unsystematically to reach its highest value of 7200 MPa at the weight ratio of 40 wt%. The decrease observed in the values of tensile strength, elongation at break and Young’s modulus for polymer blend films at some weight ratios of salt reinforcement compared with pure polymer film is due to weak interaction between the molecules and low interstitial adhesion between the composite components, which leads to an increase in the composite fragility [20].

The increase found in the values of tensile strength, elongation at break and Young’s modulus for the polymer blend films at some weight ratios

	(PVA:PVP)	15.5	28.7	332
of salt reinforcement compared with pure polymer	10	56.1	4.72	1490
film indicates that reinforcement has been achieved.	20	33.2	2.69	873
It can be concluded that, at these weight ratios,	40	12.6	0.451	7200

Figure 8: Young's modulus of pure and PVA:PVP polymer blend films reinforced with different weight ratios of CdCl<sub>2</sub>·H<sub>2</sub>O salt.

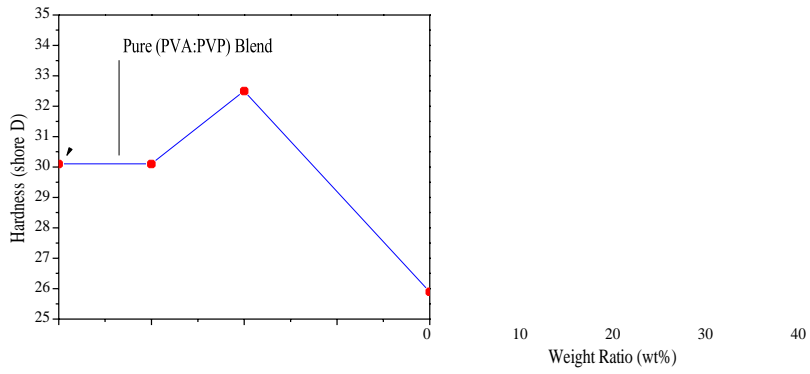
the added salt is compatible with common addition polymerization and is effectively dispersed in the polymer blend, affecting its mechanical properties [21].

*b. Hardness test*

Hardness (shore D) for pure polymer blend films and those reinforced by CdCl<sub>2</sub>·H<sub>2</sub>O salt are shown in Fig. 9. It is clear from the figure that the hardness of the pure polymer blend films increases with an increase in the weight ratio of salt added, reaching its highest value (32.5) at the 20 wt% weight ratio, and then the hardness decreases with an increase in the weight ratio of salt added. This decrease is due to the high viscosity gained by the prepared material when adding high weight ratios of reinforcing salt to the matrix (polymer blend), which is in the liquid state. The high viscosity makes penetration of the CdCl<sub>2</sub>·H<sub>2</sub>O salt inside the interfaces of the polymer blend inefficient and dif-

Table 1: Tensile property values of pure and PVA:PVP polymer blend films reinforced with different weight ratios of CdCl<sub>2</sub>·H<sub>2</sub>O salt.

Weight Ratio of Salt	Tensile Strength	Elongation at	Young's Modulus(wt %)	(MPa)	Break (%)	(MPa)
Pure						





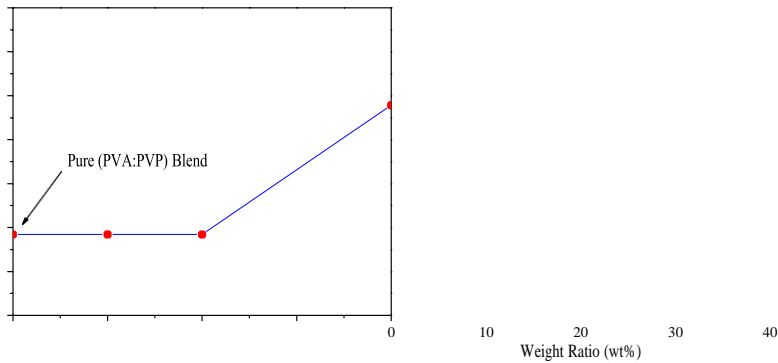


Figure 9: Hardness of pure and PVA:PVP polymer blend films reinforced with different weight ratios of CdCl<sub>2</sub>·H<sub>2</sub>O salt.

difficult, which leads to the production of many gaps within the prepared composite material when hard-ened, causing a decrease in the hardness [22]. Table 2 shows the hardness values of all polymer blend films.

*c. Impact test*

The impact test is an important mechanical test used to demonstrate the resistance of a material to collapse by the force of impact under operating conditions, as it measures the actual energy required to break a piece under the test [23].

Fracture Energy for pure polymer blend films and those reinforced by CdCl<sub>2</sub>·H<sub>2</sub>O salt were recorded at different weight ratios, as shown in Fig. 10.

It can be seen that the fracture energy value for the pure polymer blend films is 0.392 kg.m<sup>2</sup>/s, and that this value increases as the weight ratio of added salt increases. In other words, the fig-

Table 2: Hardness values of pure and PVA:PVP polymer blend films reinforced with different weight ratios of CdCl<sub>2</sub>·H<sub>2</sub>O salt.

Weight Ratio of Salt	Hardness(wt %) (Shore D)
Pure (PVA:PVP)	30.1
10	30.1
20	32.5
30	25.9

Figure 10: Fracture energy of pure and PVA:PVP polymer blend films reinforced with different weight ratios of  $\text{CdCl}_2 \cdot \text{H}_2\text{O}$  salt.

ure shows that the absorbed energy necessary for fracture increases with an increase in the weight fracture [24], where the  $\text{CdCl}_2 \cdot \text{H}_2\text{O}$  salt works to hinder the growth of the crack, and this changes the shape of the crack and its direction. This change in the shape of the crack increases the surface area of the fracture and the spent energy, all of which lead to an increase in the mechanical resistance of the material [25].

The addition of  $\text{CdCl}_2 \cdot \text{H}_2\text{O}$  salt to the PVA:PVP pure polymer blend film improved the mechanical properties. The reason for the increase in fracture energy with the increase in the weight ratio of added salt is that a large part of the impact energy projected onto the sample is reduced by the salt, which increases the resistance of the substance [25]. Table 3 shows the fractional energy values of all polymeric films.

Table 3: Fracture energy values of pure and PVA:PVP polymer blend films reinforced with different weight ratios of  $\text{CdCl}_2 \cdot \text{H}_2\text{O}$  salt.

Weight Ratio of Salt (PVA:PVP)	Fracture Energy (wt %)	( $\text{kg} \cdot \text{m}^2 / \text{s}$ )
	0.392	
10	0.392	
20	0.392	
40	0.539	

#### IV. Conclusions

When the weight ratio of  $\text{CdCl}_2 \cdot \text{H}_2\text{O}$  salt is increased at the same frequency, the dielectric constant, loss factor, and alternating electrical conductivity all rise in polymer mix films reinforced with this salt. The common consensus is that the rise in polarisation is to blame for this acceleration. The versatility of these polymer mixes makes them ideal for use in electric battery production. The tensile strength, elongation at break, and Young's modulus values of PVA:PVP polymer blend films reinforced with  $\text{CdCl}_2 \cdot \text{H}_2\text{O}$  salt vary as the salt weight ratio rises, according to the findings of the stress test. At these weight ratios, the salt is mixed with the polymer blend and has an impact on its mechanical characteristics; it is also compatible with common addition polymerisation. As the salt weight ratio increases, the hardness value first rises and subsequently falls. The produced material gains a high viscosity when large weight ratios of reinforcing salt are added to the matrix (polymer mix) when it is in a liquid condition, which is why this drop occurs. As the salt composition alters the crack's geometry and orientation, the fracture energy value rises in relation to the salt-to-weight ratio. They may be suitable for use with hard adhesives that have minimal flexibility since the altered crack form increases the fracture surface area and the energy consumed, both of which raise the material's mechanical resistance.

- [1] S A Salman, N A Bakr, S S Abdullallah, *Study of thermal decomposition and FTIR for PVA-  $\text{AlCl}_3$  composite films*, J. Eng. Appl. Sci. **14**, 717 (2019).
- [2] S A Salman, N A Bakr, M R Jwameer, *Effect of annealing on the optical properties of (PVA-CuCl) composites*, Int. Lett. Chem. Phys. Astron. **63**, 98 (2016).
- [3] B Lobo, M R Ranganath, T S G Ravi Chandran, G Venugopal Rao, V Ravindrachary, S Gopal, *Iodine-doped polyvinylalcohol using positron annihilation spectroscopy*, Phys. Rev. B **59**, 13693 (1999).

- [4] L M Robeson, *Polymer Blends Hand- book*, Springer-Kluwer Academic Publishers, Netherlands (2003).
- [5] J R Fried, *Polymer Science and Technology*, Prentice Hall Inc., Upper Saddle Rivers, New Jersey (2014).
- [6] R Singh, S G Kulkarni, *Morphological and mechanical properties of Poly(Vinyl Alcohol) doped with inorganic fillers*, Int. J. Polym.Mater. Po. **62**, 351 (2013).
- [7] P J Liu, W H Chen, Y Liu, S B Bai, Q Wang, *Thermal melt processing to prepare halogen-free flame retardant Poly(Vinyl Alco-hol)*, Polym. Degrad. Stabil. **109**, 261 (2014).
- [8] R S Mahmood, S A Salman, N A Bakr, *Op- tical, thermal properties of cadmium chloride reinforced PVA:PVP blend films*, Journal of Polymer & Composites **8**, 46 (2020).
- [9] B H Rabee, A Hashim, *Synthesis and char- acterization of carbon nanotubes-polystyrene composites*, Eur. J. Sci. Res. **60**, 247 (2011).
- [10] G C Psarras, K G Gatos, P K Karahaliou, S NGeorga, C A Krontiras, J Karger-Kocsis, *Re- laxation phenomena in rubber/layered silicate nanocomposites*, eXPRESS Polymer Letters **1**,837 (2007).
- [11] SK S Basha, M Gnanakiran, B R Kumar, K V B Reddy, M V B Rao, M C Rao, *Synthesis and spectral characterization on PVA/PVP: Go based blend polymer electrolytes*, Rasayan J. Chem. **10**, 1159 (2016).
- [12] S B Aziz, O Gh Abdullah, S A Hussein, H M Ahmed, *Effect of PVA blending on structural and ion transport properties of CS:AgNt-Based polymer electrolyte membrane*, Polymers **9**, 622 (2017).
- [13] F T M Noori, E M Mehdi, *Plasma effect on AC electrical properties of (PVA-PVP-MnO<sub>2</sub>)nano composites for piezoelectric application*, Int. J. Sci. Res. **7**, 483 (2018).



- [14] K K Verma, M S Alam, R K Sinha, R K Shukla, *Dielectric, electrical and microstructural properties of unfilled and MWCNTs filled polystyrene nanocomposite prepared by in-situ polymerization technique using ultrasonic irradiation*, Indian J. Pure Ap. Phy. **52**, 614 (2015).
- [15] M T Ramesan, V K Athira, P Jayakrishnan, C Gopinathan, *Preparation, characterization, electrical and antibacterial properties of sericin/poly(vinyl alcohol)/poly(vinylpyrrolidone) composites*, J. Appl. Polym. Sci. **133**, 43535 (2016).
- [16] R Popielarz, C K Chiang, R Nozaki, J Obrzut, *Dielectric properties of polymer/ferroelectric ceramic composites from 100 Hz to 10 GHz*, Macromolecules **34**, 5910 (2001).
- [17] S M M Stowe, Ph.D. Thesis, Department of Physics, University of Baghdad Faculty of Education - Ibn Al-Haitham, Baghdad (2005).
- [18] M B Nanda Prakash, A Manjunath, R So-mashekar, *Studies on AC electrical conductivity of CdCl<sub>2</sub> doped PVA polymer electrolyte*, Adv. Cond. Matter Phys. **2013**, 1 (2013).
- [19] X D Yu, M Malinconico, E Martuscelli, *Highly filled particulate composites enhancement of performances by using compound coupling agents*, J. Mater. Sci. **25**, 3255 (1990).

- [20] C Ravindra, M Sarswati, G Sukanya, P Shivalila, Y Soumya, K Deepak, *Tensile and thermal properties of poly (vinyl pyrrolidone)/vanillin incorporated poly (vinyl alcohol) films*, Res. J. Physical Sci. **3**, 1 (2015).
- [21] Y Luo, X Jiang, W Zhang, X Li, *Effect of aluminium nitrate hydrate on the crystalline, thermal and mechanical properties of poly(vinyl alcohol) film*, Polym. Polym. Compos. **23**, 555 (2015).
- [22] S I Salih, K M Shabeeb, Q A Hamad, *Studying mechanical properties for polymer matrix composite material reinforced by fibers and particles*, J. Tech. Univ. **4**, 81 (2010).
- [23] M C Gupta, A P Gupta, *Polymer Composite*, New Age International Publishers, New Delhi(2005).
- [24] A M Abdullah, A M Hashim, A J Bader, *Effect of alumina particles on the mechanical properties of discontinuous glass fiber reinforced unsaturated polyester composites*, Al-Qadisiyah Journal for Engineering Sciences **4**, 170 (2011).
- [25] A A Al-Jubouri, A I Al-Mousawi, KH A Ismail, A J Salman, *Effect of reinforcing by magnesium oxide particles on thermal conductivity and mechanical properties of vinyl ester resin polymer composite*, J. Karbala Univ. **Special Issue - 6th. Scientific Conference**, 26 (2010).